

Design and Manufacturing of an Attachable Power-Assist Electric Wheelchair for Mobility Enhancement of Physically Challenged Persons

Ravindra Awale¹, Akash Kumbhare², Krushanu Meshram³, Pranay Kamble⁴, Ashwini Admane^{5*}

^{1,2,3,4,5}Department of Mechanical Engineering, Shree Chanakya Education Society's Indira College of Engineering and Management, Parandwadi, Savitribai Phule Pune University, Pune, Maharashtra, India

*Corresponding Author: ashwiniphalke65@gmail.com

Peer Review Information	Abstract
Type: Article Received: 16 April 2022 Revised: 12 May 2022 Accepted: 15 June 2022 Published: 05 July 2022	Manual wheelchair propulsion causes severe physical fatigue and limits long-distance autonomy for lower-limb impaired individuals. This research presents the end-to-end design, kinematic modeling, FEA verification, and fabrication of a quick-attach front-drive electric assist kit that converts standard manual wheelchairs into powered tricycles. Driven by a 24 V, 350 W BLDC hub motor powered by dual 12 V, 7.2 Ah lead-acid batteries, the system generates 206.35 W required drive power to achieve 16 km/h under 100 kg total payload on an 2 °C incline. Structural stress and FEA evaluations yield a minimum Factor of Safety (FOS) of 1.528. Total prototype fabrication cost was ₹23,190. Keywords: Electric Wheelchair; Power-Assist Mechanism; BLDC Hub Motor; Structural Analysis; Kinematic Modeling.

How to Cite This Article

Awale, R., Kumbhare, A., Meshram, K., Kamble, P., & Admane, A. (2022). Design and manufacturing of an attachable power-assist electric wheelchair for mobility enhancement of physically challenged persons. *International Journal on Mechanical Engineering and Robotics*, 11(1), 1–5.

Introduction

Worldwide, an estimated 10% of individuals with disabilities require a wheelchair for daily locomotion. Standard manual wheelchairs impose high metabolic strain, leading to upper-limb joint degradation and caregiver fatigue. Commercial electric wheelchairs solve these physical limitations but remain financially inaccessible in developing regions. This work introduces a low-cost, quick-attach front-drive power-assist unit that clamps directly onto standard manual wheelchairs without structural alterations.

Literature Review

Prior studies highlight the efficacy of modular electric attachments in lowering financial barriers and improving autonomy:

Vigneshwar et al. & Shaikh et al, demonstrated that attachable direct-drive hub motors minimize mechanical vibration, reduce transmission loss, and improve outdoor transit.

Jayaprabakar & Sidik et al, Emphasized low center-of-gravity design, ground clearance, and the psychological benefits of independent personal mobility.

Kumbar et al. & Khatib, confirmed that modular front-wheel propulsion offers superior indoor maneuverability combined with stable outdoor transit.

Binismail, Identified critical stress concentrations across wheelchair seating frames and front casters during obstacle negotiation.

Research Gap & Novelty

Existing solutions are either cost-prohibitive, excessively heavy (30–50 kg), or require permanent chassis modification. The key novelties of this design are:

1. Dual-Mode Attachment: Quick-detach clamp mounting in under two minutes without modifying the base wheelchair frame.
2. Integrated Drive-Steer Hub: Direct integration of a 24 V, 350 W BLDC hub motor into a single front assembly.
3. Rigorous Design Validation: Analytical dynamic force calculations paired with finite element displacement verification.

Objectives

- Design and prototype an attachable electric drive unit that connects to standard manual wheelchairs.
- Derive analytical force equations for total vehicle motion resistance (rolling, gradient, and aerodynamic drag) to size the electric motor and battery bank accurately.
- Perform Finite Element Analysis (FEA) on the primary steering handle structure to determine factor of safety and deformation patterns.
- Complete prototype assembly and cost estimation to confirm financial viability.

System Specifications

Table 1. Overall Wheelchair Specification Parameters

Parameter	Value / Specification
Overall Dimensions (L*W * H)	1150 (mm* 660(mm) *910(mm)
Rear Wheel / Castor Wheel Diameter	24 inch / 12 inch
Seat-to-Ground Height / Backrest Height	480(mm)* 460(mm)
Push Rim Diameter	18 inch

Mathematical Modeling & Governing Equations

The total resistive force $F(\text{Total})$ acting on a 100 kg system ($m = 100\text{kg}$) moving at $v = 16\text{km/h}$ 4.44m/s is:

$$F\{\text{Total}\} = F\{\text{Rolling}\} + F\{\text{Gradient}\} + F\{\text{Aerodynamic Drag}\}$$

1. Rolling Resistance Force ($C_r = 0.004$):

$$F\{\text{Rolling}\} = C_r * m * g = 0.004 * 100 * 9.81 = 3.924 \text{ N} \dots\dots\dots(1)$$

2. Gradient Resistance Force ($\theta = 2^\circ$ incline):

$$F\{\text{Gradient}\} = m \cdot g \cdot \sin(\theta) = 100 \cdot 9.81 \cdot \sin(2^\circ) = 34.236 \text{ N} \dots \dots \dots (2)$$

3. Aerodynamic Drag Force ($\rho = 1.23 \frac{\text{kg}}{\text{m}^3}$ $C_a = 0.88$, $A_t = 0.7917 \text{ m}^2$)

$$F\{\text{Aerodynamic Drag}\} = 0.5 \rho V^2 \cdot C_a \cdot A_t = 0.5 \cdot 1.23 (4.4^2) \cdot 0.88 \cdot 0.7917 = 8.27 \text{ N}$$

4. Total Force & Power Requirement:

$$F\{\text{Total}\} = 3.924 + 34.236 + 8.27 = 46.43 \text{ N}$$

$$P\{\text{req}\} = F\{\text{Total}\} \cdot V = 46.43 \text{ N} \cdot 4.44 \text{ m/s} = 206.35 \text{ W}$$

The calculated power demand 206.36 W is well within the 350 W rating of the chosen motor.

Motor Kinematics & Current Draw

- Nominal Current Draw I: At 24 V rating, $I = 350 \text{ W} / 24 \text{ V} = 14.58 \text{ A}$.
- Wheel Angular Speed (N): For wheel radius $r = 0.155 \text{ m}$ (circumference $C_w = 0.9734 \text{ m}$), top speed 333 m/min requires:
 $N = 333 \text{ m/min} / 0.9734 \text{ m/rev} = 342 \text{ RPM} \dots \dots \dots (1)$
- Shaft Torque Output (T):**
 $T = 60 P / 2\pi \cdot N = 60 \cdot 350 / 2 \cdot \pi \cdot 342 = 14.73 \text{ N m}$

Battery Storage & Charging Kinetics

- Capacity Requirement: Operating a 350 W motor for 1 hour requires 350 Wh, translating to $AH = 350 \text{ Wh} / 24 \text{ V} = 14.58 \text{ Ah}$.
- Charging Kinetics: Setting safe charging current at 30% capacity ($I_c = 0.3 \cdot 14.58 = 4 \text{ A}$), estimated charge time is $T_c = 14.58 / 4 =$ approx 3.65 hours (operational benchmark accounting for efficiency losses is ~4.98 hours).

Steering Kinematics & Turning Radius

For wheelbase $W_b = 0.94 \text{ m}$ and maximum steering angle $\alpha = 70^\circ$:

$$R(\text{front}) = W_b / \sin(\alpha) = 0.94 / \sin(70^\circ) = 1.003 \text{ m} \dots \dots \dots (1)$$

$$r\{\text{rear}\} = W_b / \tan(\alpha) = 0.94 / \tan(70^\circ) = 0.3421 \text{ m} \dots \dots \dots (2)$$

Page 4: Mechanical Structural Analysis

Structural Stress Calculations

Table 2. Mechanical Properties of Shaft Steel (C45 Grade)

Property	Value
Tensile Strength / Yield Strength	655 MPa / 415 MPa
Elastic Modulus / Poisson's Ratio	190–210 GPa / 0.27–0.30

Hollow Motor Shaft ($D_o = 15 \text{ mm}$ $d_i = 6 \text{ mm}$ $L = 20 \text{ mm}$)

$$Z_{\text{shaft}} = \pi (15^4 - 6^4) / (32 \cdot 15) = 102.77 \text{ m}^3 \dots \dots \dots (1)$$

$$W_{\text{allow}} = (\sigma_b \cdot Z_{\text{shaft}}) / L = 655 \cdot 102.77 / 20 = 3365.71 \text{ N} (342.9 \text{ kg}) \dots \dots \dots (1)$$

The allowable shaft load (3365.71) far exceeds the applied static load (981 N).

Steering Handle Hollow Tube ($D_o = 20 \text{ mm}$, $d_i = 17 \text{ mm}$, $L = 250 \text{ mm}$)

$$Z_{\text{pipe}} = \pi (20^4 - 17^4) / 32 \cdot 20 = 375.41 \text{ m}^3$$

For C45 steel ($\sigma_{\text{allow}} = 270 \text{ MPa}$), allowable handle bar force is $W = 270 \cdot 375.41 / 250 = 405.44 \text{ N} (41.3 \text{ kg})$.

Steering Handle Solid Shaft ($d = 20 \text{ mm}$, $L = 215 \text{ mm}$)

$$Z_{\text{solid}} = \pi \cdot 20^3 / 32 = 785 \text{ m}^3 \quad W_{\text{solid}} = 270 \cdot 785 / 215 = 985.81 \text{ N} (100.4 \text{ kg}) \dots \dots (1)$$

Fastener Bolt Tension (M10, Root $d_c = 8 \text{ mm}$)

$$\text{Sigma-bolt} = 981 \text{ N} / (\pi/4 \cdot 8^2) = 19.51 \text{ N/mm}^2 \text{ } (<<420 \text{ N/mm}^2 \text{ yield point}) \dots\dots(1)$$

Chassis Tube Section (25 mm *25 mm *3 mm)

$$Z_{\text{square}} = (25^3 - 19^3) / 6 = 1461 \text{ mm}^3 \quad W_{\text{chassis}} = 270.146 / 250 = 1577.88 \text{ N (160.7 kg)}$$

Page 5: Structural Schematics & CAD / FEA Verification

System Component Layout

- Structural Layout: Padded seat frame, push handles, 24-inch rear wheels with 18-inch push rims, and dual front caster wheels.
- Drive Assembly: Detachable T-bar handle housing twist-throttle, controller, dual 12 V SLA batteries, and 6-inch BLDC front hub motor.
- Bearing Support: P204 pedestal bearing unit (20mm bore) securing the solid steering column.

Finite Element Analysis (FEA) Results

Static stress and displacement simulations were conducted on the T-bar handle structure under maximum load vectors in SolidWorks Simulation:

- Elastic Displacement (U_{RES}): Zero displacement at fixed constraint nodes; maximum deflection of 0.8144 mm at the outer handle tips.
- Factor of Safety (FOS): Minimum localized FOS recorded at 1.528 (critical node 11072), proving high structural stability under maximum operating conditions.

Page 6: Fabrication Cost Analysis & Performance Evaluation

Component & Fabrication Cost Estimation

Table 3. Complete Prototype Cost Breakdown

Item Description	Specification / Material	Qty	Cost (INR ₹)
Standard Wheelchair Base	Steel Tubular Chassis	1 Unit	5,000
Electric Hub Motor	24 V, 350 W BLDC	1 Unit	9,000
Lead-Acid Batteries	12 V, 7.2 Ah SLA	2 Units	2,200
Motor Controller	24 V PWM Unit	1 Unit	1,800
Mild Steel Profiles & Shafts	C45 Mild Steel Square/Round Tubes	8 kg	1,080
Steering Bearings (P204)	Pedestal Ball Bearings	2 Units	800
Fasteners, Charger & Wiring	M10 Bolts, AC Charger, Copper Cables	Various	1,290
Throttle, Paint & Fabrication	Twist Throttle, Coating, Shop Labor	Various	1,720
Total Fabrication Cost			₹23,190

Experimental Validation

- Speed & Range: Reached a top speed of 16 km/h with a 16 km single-charge operating range under 100 kg load.
- Attachment Capability: Quick-clamping interface enables attachment/detachment in under 2 minutes.

Page 7: Future Scope, Conclusion & References

Future Improvements

- Intelligent Assist Integration: Incorporating voice-command or BCI sensor modules for quadriplegic users.
- LiFePO4 Battery Upgrade: Switching to Lithium Iron Phosphate batteries to reduce pack weight by >50%.
- Active Safety: Integrating ultrasonic range sensors and automated collision avoidance.

Conclusion

This project successfully demonstrates a low-cost, quick-attach electric power-assist module for manual wheelchairs. Mathematical dynamic modeling verifies that a 350 W BLDC hub motor fulfills all power requirements (206.36 W required) up to 16 km/h on 2° slopes. Bending stress calculations and FEA simulation establish structural safety with a minimum Factor of Safety of 1.528. At a fabrication cost of ₹23,190, this system offers an effective and accessible mobility solution for developing regions.

Nomenclature

- At: Frontal Area ($0.7917m^2$)
- Ca / Cr: Drag Coeff. (0.88) / Rolling Coeff. (0.004)
- F_{Total}: Total Resistive Force (N)
- P_{req}: Required Power Output (W)
- Z: Elastic Section Modulus (m^3)
- σ_{allow} : Allowable Design Stress (N/ mm^2)

Abbreviations

- BLDC: Brushless Direct Current
- FEA: Finite Element Analysis
- FOS: Factor of Safety
- PWM: Pulse Width Modulation
- SLA: Sealed Lead-Acid

References

1. M. Reddi Sankar et al., "Design and Development of Solar Assisted Bicycle," *IJSRP*, vol. 3, no. 3, 2013.
2. R. C. Simpson, "Smart wheelchairs: A literature review," *JRRD*, vol. 42, no. 4, pp. 423–438, 2005.
3. S. Yadav and P. Sheoran, *IJIERT*, vol. 3, no. 2, pp. 12–18, 2016.
4. Varun N., "Power Assist Wheelchair for Physically Challenged Person," *JETIR*, vol. 8, no. 8, 2021.
5. A. Shaikh, "Handcycle Attachment for Wheelchair," *IRJMETs*, vol. 3, no. 2, 2021.
6. Rollick, "Products - Firefly Electric Attachable Bike," 2016.
7. N. Agarwal et al., "Combination hand and electric tricycle," *NSF Grantee Conf.*, 2007.